

# Heat Load Calculations

- I started trying to make a spreadsheet that could model the heat load with varying parameters of the mechanical design
- There were certain assumptions made, and loading modes that were ignored for simplicity, but may be significant, and I wanted to include these.

# Convection

- All calculations of heat flow until now have used the assumption of an infinite heat bath at  $T_{\text{amb}}$
- There is a limit due to the lousy conductivity of air to the amount of heat that can be supplied through a given area, known as  $h$  the convective heat transfer coefficient.
- For free convection in air, this ranges from 1 to 30 W/m<sup>2</sup>/K.
- This constrains the heat flow, and allows the determination of the temperature of the edge of the board, and the “warm” side of the fiber connector.

# The Cookie

- Assuming the cookie is 15mm x 15mm and 10mm thick.
- Assuming  $Q = kA/L * (T_h - T_c)$  and using  $T_h = T_{amb}$  would yield  $0.33 \text{ W/m/K} * 225 \text{ E-}6 \text{ m}^2 / 0.01 \text{ m} (25 - (-15)) = 0.297 \text{ W}$
- However, given  $Q = hA(T_{amb} - T_h)$ , and a high  $h$  of  $30 \text{ W/m}^2/\text{K}$  would require a  $dT$  of  $0.297 / 30 / 225 \text{ E-}6 = 44 \text{ K}$  -- TOO LARGE
- Instead use the equations to calculate  $T_h$ , the temp of the *hot* side of the cookie and then determine  $Q$
- $kA/L * (T_h - T_c) = hA(T_{amb} - T_h)$
- $T_h = (h * T_{amb} + k/L * T_c) / (k/L + h)$
- For this example,  $T_h = 4 \text{ C}$ , and  $Q = 0.14 \text{ W}$ , not 0.297
- If  $h$  is lower, this value is reduced further.

# The Board

- Assuming a board is 40mm x 40mm and 1.52mm thick.
- A brute force calculation assuming  $k=0.62\text{W/m/K}$  and a 15mm x 15mm APD at  $-15$  at the center yields power of 0.25W
- Approximating the area of the board as a circle of circumference  $\pi*L$  with thickness of 1.52mm given  $Q=hA(T_{\text{amb}}-T_h)$ , and a high  $h$  of  $30\text{W/m}^2/\text{K}$  would require a  $dT$  of  $0.25/30/(3.14*40*1.52\text{E}-6)=44\text{K}$  --TOO LARGE
- Instead use the equations to calculate  $T_h$ , the temp of the *hot* side of the board and then determine  $Q$
- $kA/L*(T_h-T_c)=hA(T_{\text{amb}} - T_h)$
- $T_h=(h* T_{\text{amb}} +2k/L* T_c)/(2k/L+h)$
- For this example,  $T_h=5\text{C}$ , and  $Q=0.12\text{W}$ , not 0.25
- If  $h$  is lower, this value is reduced further.

# What Else?

- Convection and Radiation between the board and the heat sink in areas that are not covered with the APD
  - The area of the hot plate and board are  $(40\text{mm} \times 40\text{mm} - 15\text{mm} \times 15\text{mm}) = 0.0014\text{m}^2$
  - The convection loss heats the air and the air heats the board, this is  $30 * 0.0014 * 15 = 0.63\text{W}$ !
  - Radiation loss is  $5.67\text{E}-8 * 0.0014 * (288^4 - 258^4) = 0.2\text{W}$